

Force Measurement on Aircraft Model with and without Winglet using Low Speed Wind Tunnel

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Abstract--The objective of the research is to conduct experiment by fabricating a standard aircraft model and retrofit winglets with cant angles 0 degree (vertical), 30 degree and 60 degree. The experiments were conducted in a subsonic wind tunnel of size (feet) 3x4x6. The experiment was conducted both for basic model and the model modified with winglets. The model with winglet has exhibited substantial reduction of coefficient of drag. The stall characteristics of the winglet were analyzed by plotting suitable graph. A calibrated three component balance was used for measuring the forces. Automated turntable mounted in the test section of the wind tunnel and the recording systems were used efficiently. The results were compared and discussed.

Keyword: Aircraft model, Wind tunnel, Winglet, Vortex, Lift, Drag

NOMENCLATURE

C_A	axial force Coefficient
C_N	normal force Coefficient
C_L	lift Coefficient axial
C_D	drag Coefficient
C_M	pitching moment Coefficient
C_S	side force Coefficient
C_Y	yawing moment Coefficient
ρ	Density of air kg/m ³
V	Velocity of free stream air m/s
α	Angle of Attack (AOA)
q	Dynamic pressure
c	Chord length in mm
Re	Reynolds number
L	Length of the model (m)
L_{ref}	Reference length of the model

I. INTRODUCTION

It has been a constant endeavor by aviation enthusiasts to improve the wing efficiency. The design of aircraft is limited by the constraints of weight and geometrical feature of aspect ratio. Therefore, any addition or modification to the existing aircraft or in the new design has to be seen in this perspective. In the conventional aircraft the wing tip vortices are responsible for the induced drag due to lower pressure at the upper surface of wing and higher pressure at the lower surface of the wing. The trailing vortices at the wing tip are formed due to airflow caused by the differential pressure below and top of the wing. This is the primary cause for the induced drag which is in the range of about 20% of total drag. To alleviate this problem the researchers have come out with the optimum solution by introduction of devices to overcome the wing tip vortices. Whitcomb was the pioneering researcher in this field of winglet. In his experimental work he has established the wing efficiency has improved by 9% and reduction of drag by 20%. The reduction of induced drag will enhance the range of

aircraft, performance improvement in handling of aircraft and the cost of operation by saving fuel. The designers has experimented different devices for lift enhancement like wing end plates, upper winglet, lower winglet and multiple winglets. The winglet has become usual phenomena for commercial aircraft in the recent days. The aircrafts all over the world are commercially adopting winglet technology for fuel saving to effect profitable cost of operation.

II. REDUCTION OF INDUCED DRAG

The induced drag is vital portion of the total components of drag. Any reduction in the induced drag will substantially augment the lift which is essentially needed for aircraft during crucial role of climb. The induced drag is essentially created due to pressure difference between upper and lower surface of the wing. The trailing vortex at the wing tip is the instrumental cause for creation of induced drag. The effort is suitably arrest the creation of vortices by installing winglet at the wing tip.

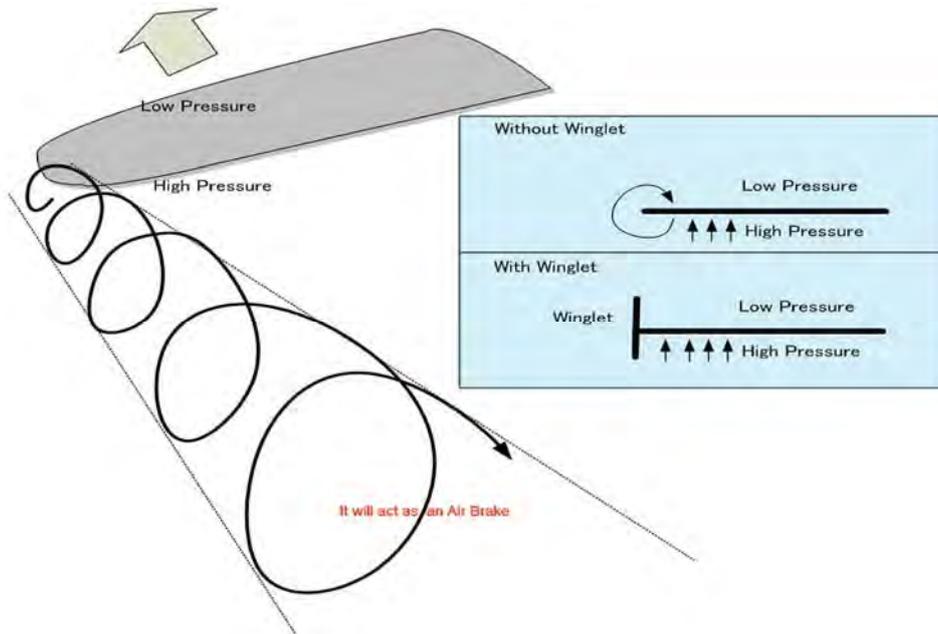


Fig 1. Vortex formation and Reduction of Induced Drag

III. EXPERIMENTAL SETUP

The experiment was conducted at subsonic wind tunnel at Madras Institute of Technology, Chennai, India. It has test section 3 ft × 4 ft and of suction type wind tunnel. The maximum rpm attained by the drive is 1500. The experiments were conducted at rpm range from 300 to 600. Higher rpm was avoided to prevent possible vibration which may lead to inaccurate readings. The aircraft model was mounted in the test section using the automated model mounting mechanism. The automated model mounting mechanism provides both pitching and yawing movement independently. These can be measured for different pitch angles and different electric motor propeller rpm. The model independent movements in pitch (keeping yaw constant) are controlled using a digital TED (touch enabled display) control panel connected to automated mounting mechanism.



Fig 2. Aircraft model with winglet mounted in the wind tunnel test section

IV. THREE COMPONENT STRAIN GAGE BALANCE

The three component balance is an integral RAE type with a maximum diameter of 15mm and length of 210 mm. It is made out of alloy steel 17-4-PH. This has yield strength of 120 Kg/mm² and UTS of 120 Kg/mm². The balance consists of two normal force gage stations for determination of normal force, pitching moment and two axial force measuring bridges. The two axial force measuring bridges are externally connected in parallel to give one common averaged output. Balance center is located at the center of the two normal force measuring units. All gage stations are of bending type. Four strain gages are bonded to each of the gage station to form four active arms of Whetstone Bridge.

The load specifications for the balance are

Axial Force(X direction) 20N (2Kg)

Normal Force(Y direction) 60N (6Kg)

Pitching Moment about Z axis 4.5 Nm (450Kgmm)

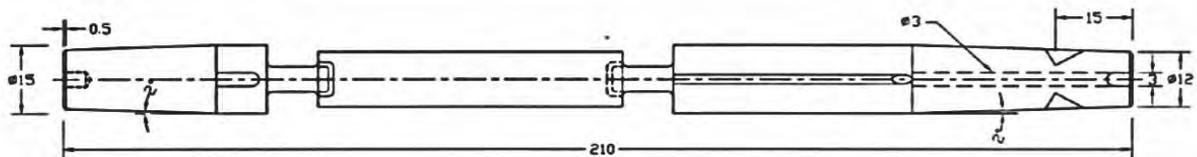


Fig 3. Schematic diagram of internal three component balance

The balance has been calibrated using calibration test rig facility available at MIT ,Chennai. It was done for very low loads so that the accuracy of results will be high enough to pick up minute forces during the wind tunnel test. The load range used for calibration is as follows.

Axial loading (AF) 0.5 kg (in steps of .05g)

Normal Force (N1) 0.5 kg (in steps of .05g)

Normal Force (N2) 0.5 kg (in steps of .05g)

From the calibration values the inverse co-efficient matrix had been calculated

TABLE I
Inverse coefficient Matrix

O/pLoad--->	AF	N1	N2
AF	2.174596	0.048832	-0.00299
N1	0.022949	3.032325	-0.07365
N2	-0.00879	0.012563	3.098821

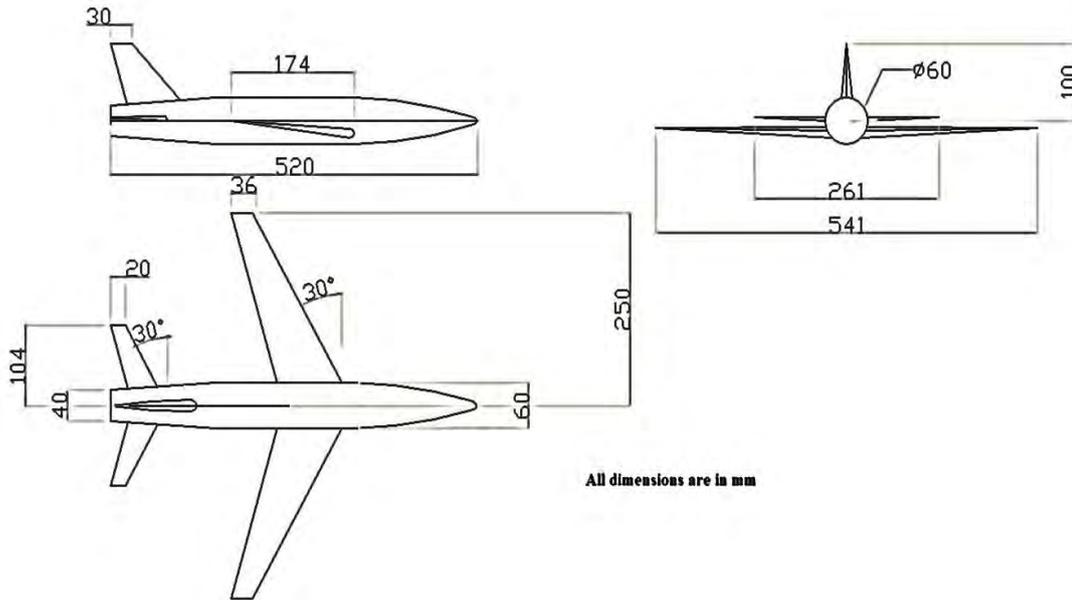


Fig 4.Aircraft model with three dimensional view

In this experiment, wing-body-tail model with and without winglets of suitable scale is fabricated to fit in the test section of the low speed subsonic wind tunnel so as to keep the blockage ratio below 5%. These models are used as standard for checking and controlling the new wind tunnel installations. The model has adequate internal space for setting up three component wind tunnel balance with diameter of 15mm. Airfoils of the wing and airfoils of the horizontal and vertical tails are symmetrical with maximum thickness of 10.5 % at the 37.5% of the chord. Aspect ratio of the wing is 7.31, and its installation angle is 3° with relation to the fuselage axis. It is made into three parts with nose, wing body and the tail assembly. A metallic insert is given to tail part where the adaptor is to be fixed. Winglet has root chord 30mm, tip chord 15mm, sweep angle 40 degrees and height 25 mm. The cant angle is measured with reference to vertical axis. The experiments were conducted for cant angles 0degree (vertical winglet), 30 degrees and 60 degrees.

V. DATA ACQUISITION SYSTEM

Spider 8-30 is the data acquisition system used for electric measurement of mechanical variables such as strain, force, pressure, path, acceleration and for temperatures. It uses 600 Hz carrier frequency amplifier to manage all measurement tasks with S/G in quarter, half or full bridge connection. All the signal conditioning excitation for passive transducers and amplification, digitization, computer interface and connection technology for a maximum of 8-channels is combined in one-housing. Each channel works with a separate A/D converter which allows measuring rates from 1/s to 9600/s. This means that Spider8 covers the entire range of mechanical measurement tasks. CATMAN professional is the software package used to obtain the aerodynamic forces and moments as a function of time. The following formulae were used for calculation.

Calculation of coefficient of lift and drag

$$\text{Coefficient of lift } (C_L) = C_{N \cos \alpha} - C_A \sin \alpha$$

$$\text{Coefficient of drag } (C_D) = C_A \sin \alpha + C_{N \cos \alpha}$$

$$\text{Coefficient of axial force } (C_A) = \frac{AF}{q_\infty * S_{ref}}$$

$$\text{Coefficient of normal force } (C_N) = \frac{(N_1 + N_2)}{q_\infty * S_{ref}}$$

VI. RESULTS AND DISCUSSION

The results of the experiment were plotted for analysis and comparison. The comparison graphs are made by keeping the yaw angle constant. The variation was done on the pitch angle and the free stream velocity. The angles tested were from -8 degrees to +16 degrees in the step of 4 degrees. The velocities tested were from 8 m/s to 24 m/s in the steps of 4m/s. The parametric variation for winglet tested were for cant angles 0 (vertical winglet), 30 and 60 degrees.

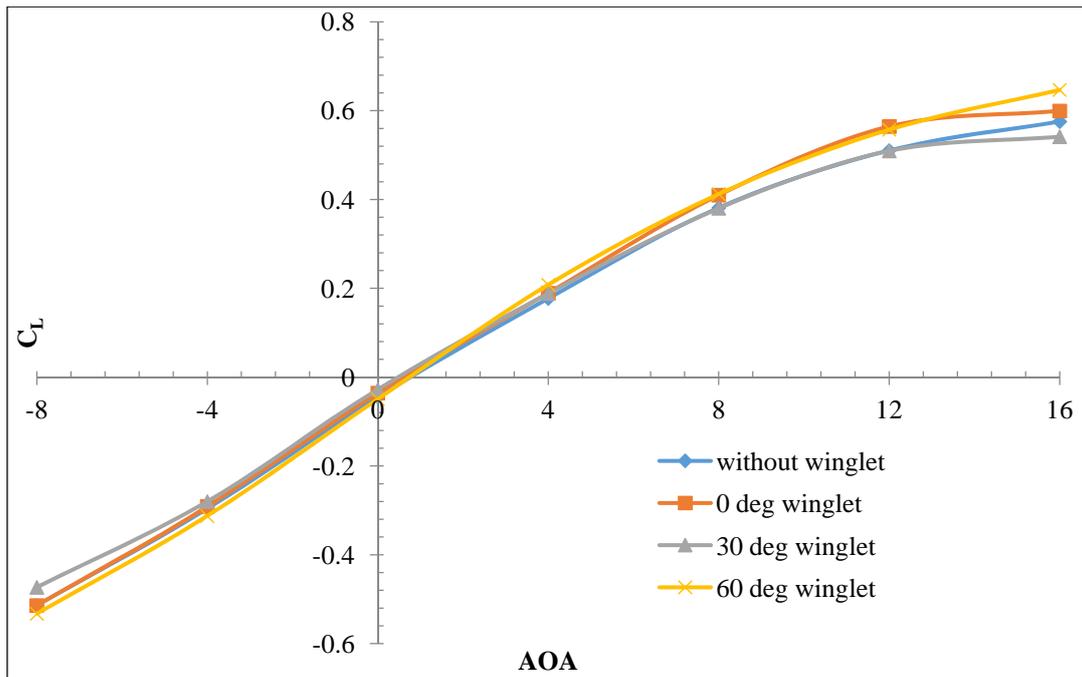


Fig 5. Lift coefficient Vs pitch angle at 8 m/s

The graph is plotted for coefficient of lift Vs pitch angle for different winglet cant angles at velocity 8 m/s. The winglet configurations has higher coefficient of lift compared to model without winglet. Vertical winglet and 60 degree winglet are showing significant rise in C_L compared to basic model. At negative angles of attack the 30 degree winglet is showing higher lift compared to other configurations.

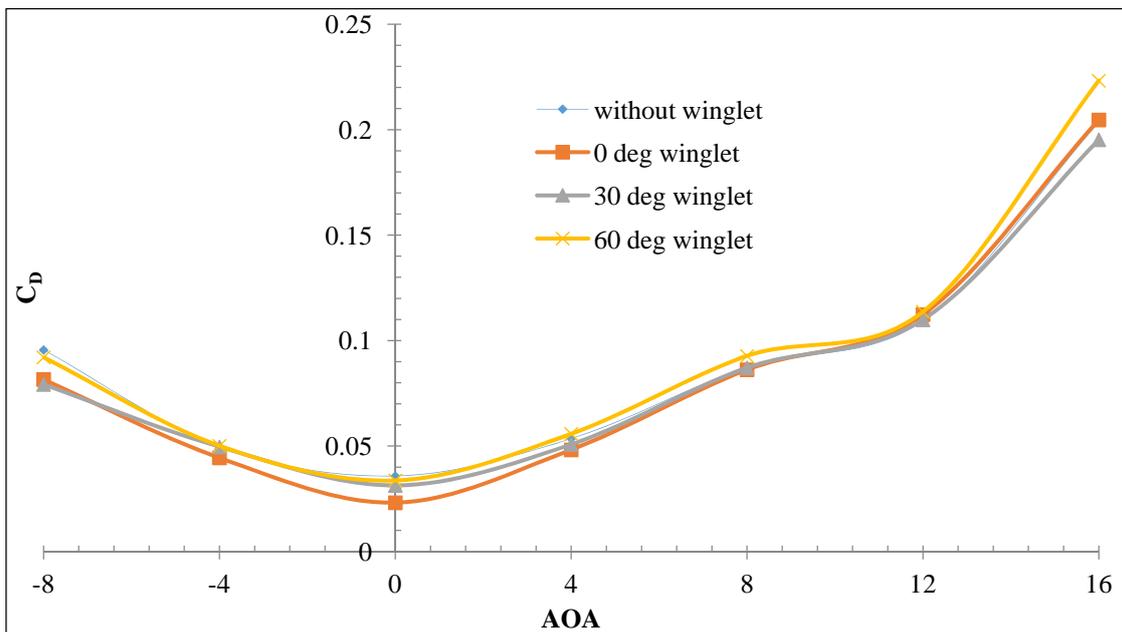


Fig6. Drag coefficient Vs angle of attack at velocity 8 m/s

The graph is plotted for coefficient drag and pitch angles. The drag coefficient graph is drawn at velocity 8 m/s. The graph shows substantial reduction in the drag for the model fitted with different winglet cant angles. The vertical winglet exhibits more drag reduction compared to other winglets. At high angles of attack the 30 degree winglet is exhibiting lowest drag.

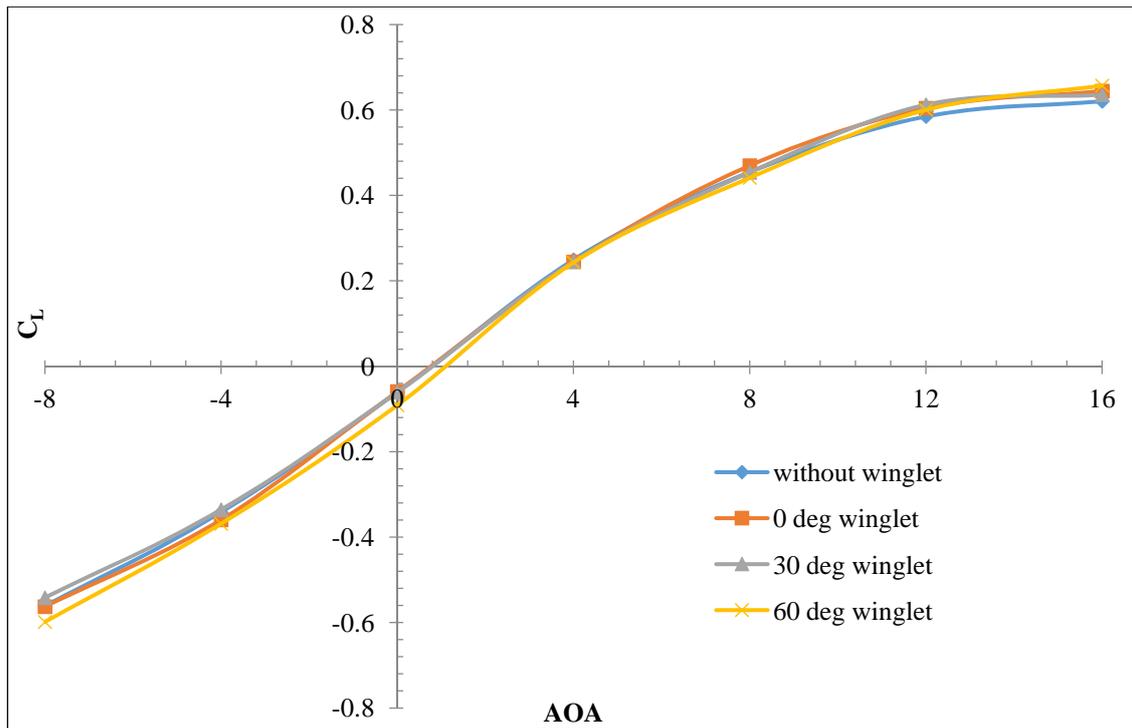


Fig 7. Lift coefficient Vs pitch angle at 12m/s

The plot is drawn for velocity at 12m/s. At this velocity the winglet with 60 degrees showing increased lift coefficient compared to other winglet configurations. This is more noticeable at high angles of attack.

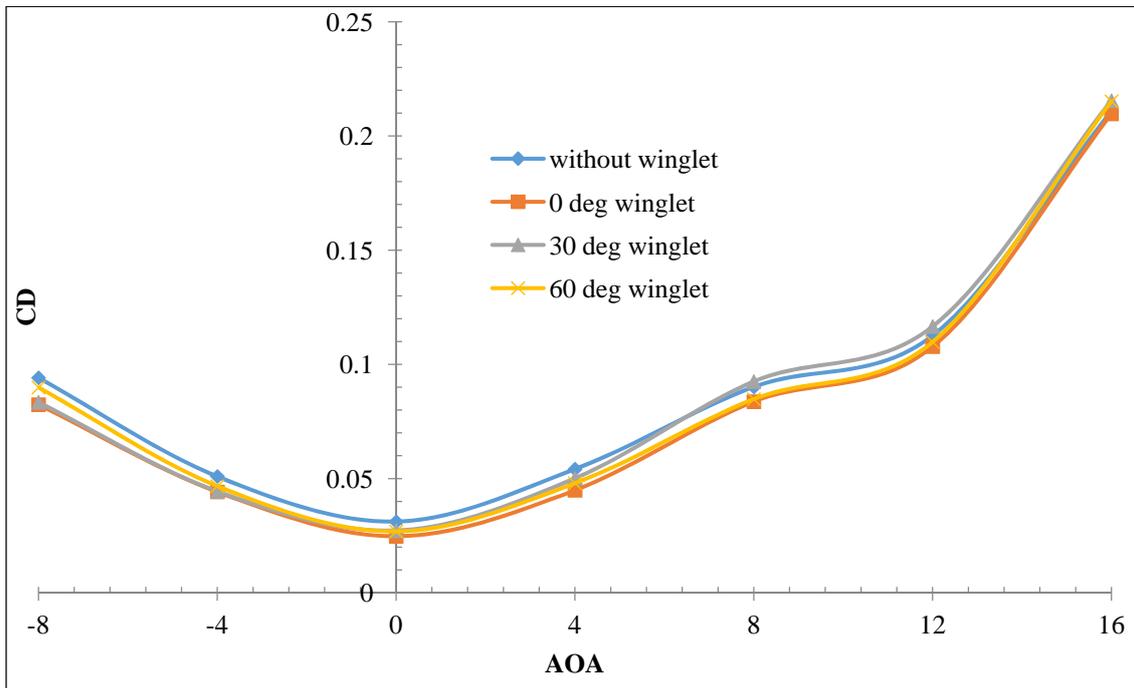


Fig 8. Drag coefficient vs angle of attack at velocity 12 m/s

The plotting is done for wind tunnel velocity of 12m/s. The coefficient of drag for the winglets with different configurations are lesser compared to the basic model. It once again reinforces that the winglet produces decrease in drag compared to the model without winglet.

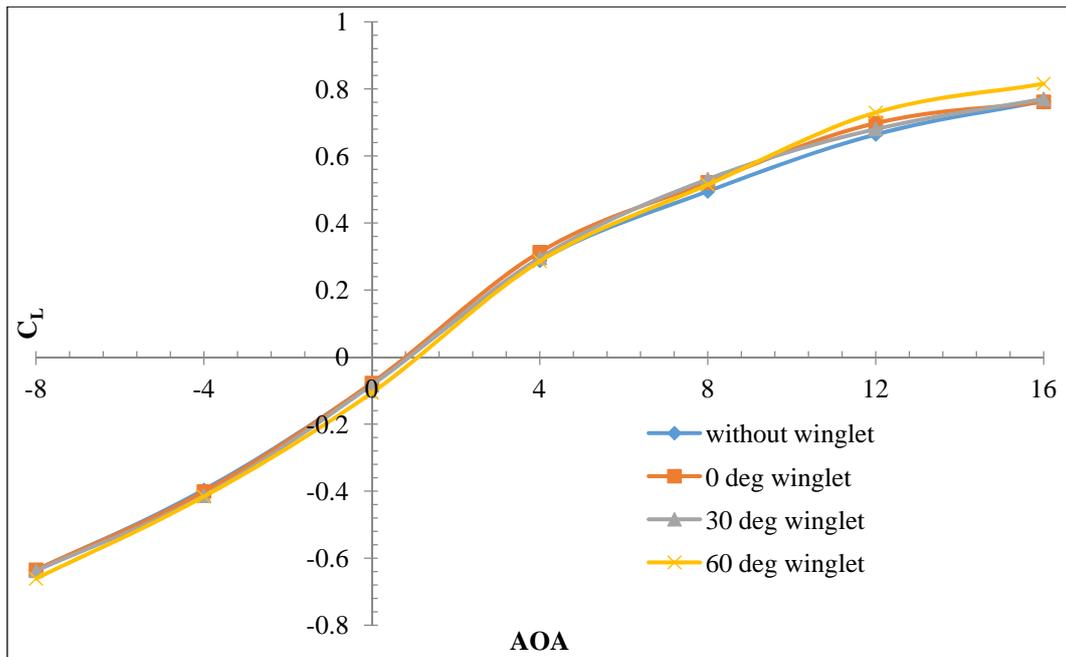


Fig 9.Lift coefficient Vs pitch angle at velocity 16m/s

At velocity 16m/s for the negative angles of attack not much variation in C_L is exhibited. At higher angles attack the winglet performance is noticeable in increasing lift coefficient compared to basic model.

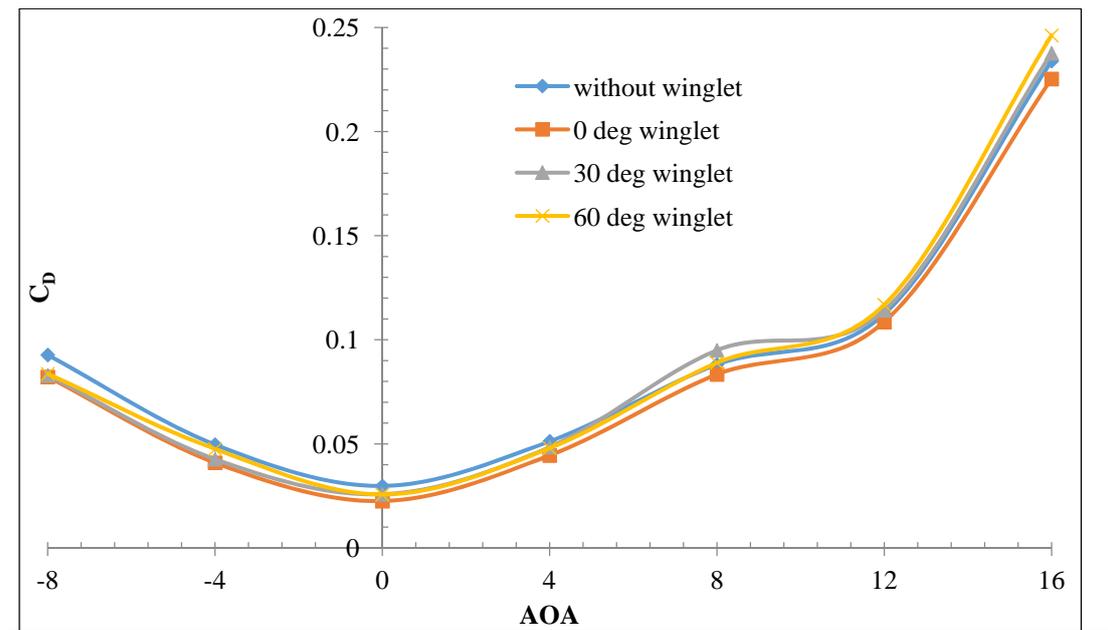


Fig10. Coefficient of drag Vs angle of attack at velocity 16m/s

The graph is plotted for velocity at 16 m/s. Around 8 degrees sudden increase in drag of basic model is noticed. The winglets are contributing to reduction of drag as exhibited in the graph.

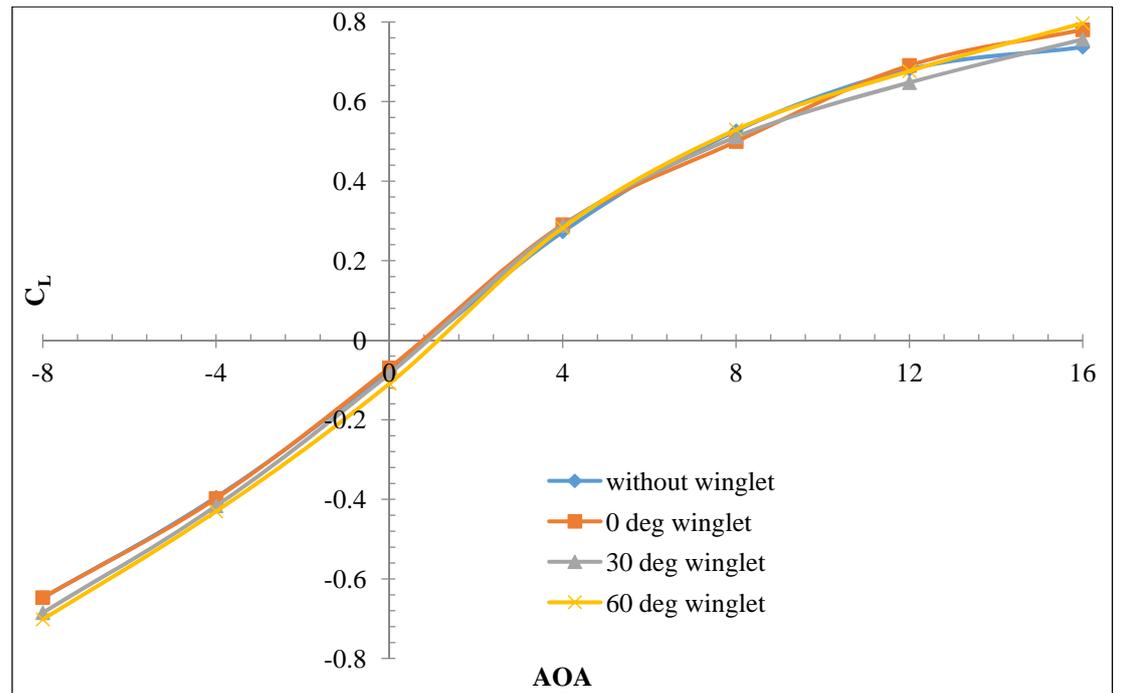


Fig11. Lift coefficient Vs pitch angle velocity at 20 m/s

The graph is plotted for velocity at 20 m/s. throughout the range of angles of attack the vertical winglet is showing high lift coefficient. Around 16 degrees of angle of attack, the pattern of graph for winglets are different. The basic model has tendency to stall at high angle of attack is observed.

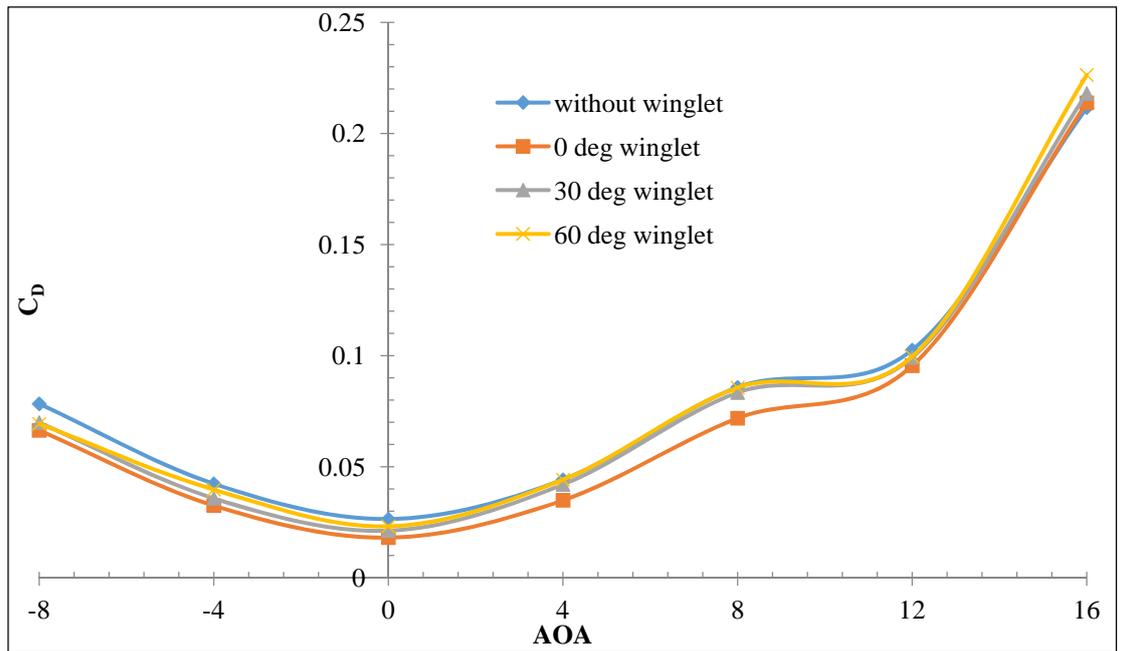


Fig. 12. Drag coefficient Vs angle of attack at velocity at 20 m/s

The graph plotting is done for the wind tunnel speed at 20m/s. At high velocity the coefficient of drag for different winglet are distinctly noticed. The vertical winglet continues to exhibit low drag coefficient compared to the other winglets throughout the range of angles of attack.

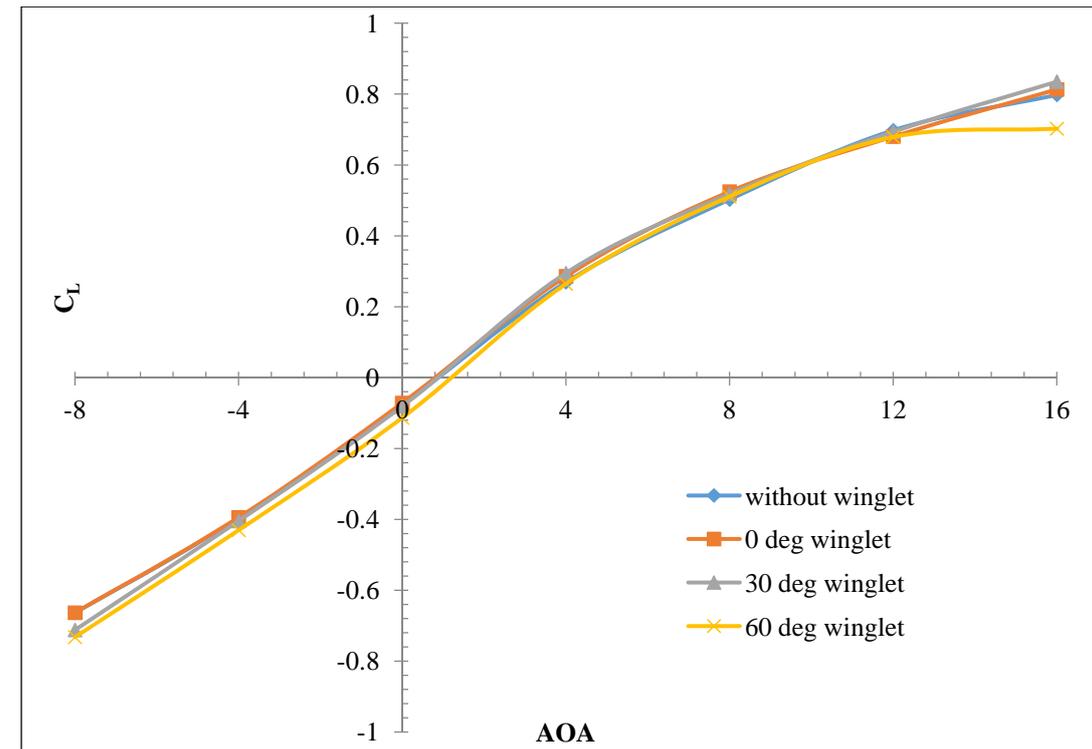


Fig 13. Lift coefficient Vs pitch angle for velocity at 24m/s

The coefficient of lift is showing similar trend for all winglet configurations. The winglet with 60 degree is showing stall characteristics at high angle of attack. The basic model also has tendency to stall at high angle of attack. This is continuation of what was noticed at 20 m/s for lift curve. The winglet with 30 degree cant angle has improved stall characteristics.

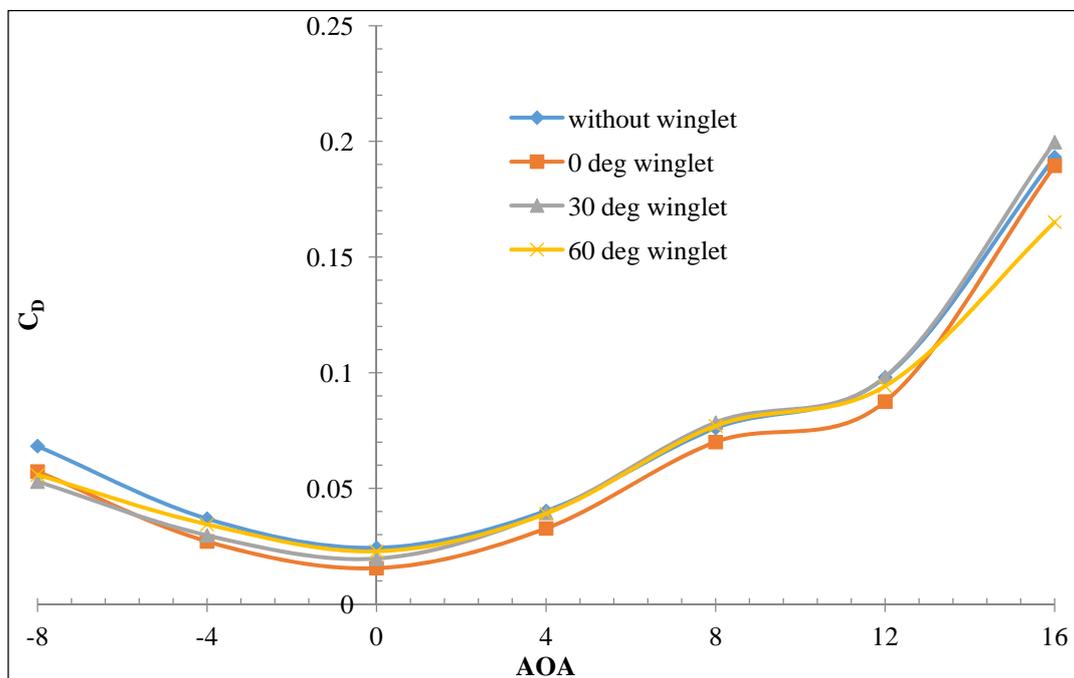


Fig 14. Drag coefficient Vs pitch angle for velocity at 24 m/s

The graph is plotted for subsonic speed of 24 m/s. The graph shows sustained trend of reduction of coefficient of drag for different cant angles at 24 m/s. The winglet with 60 degree shows high slope of drag compared to other winglet configurations. The basic model also exhibits high slope dragcoefficient indicative of stall characteristics.

VII. CONCLUSION

The experimental investigation of winglet effects on aircraft model were conducted at subsonic wind tunnel. The parametric three variation of winglet angles were chosen for the model. The testing was done for the basic model and winglet having cant angles 0 (vertical winglet), 30 and 60 degrees. The testing was done for pitch angle varying from -8 degrees to +16 degrees. The models were tested at speeds ranging from 8 m/s to 24 m/s in steps of 4m/s. The vertical winglet contribution of coefficient of lift was significant. It has been observed at high speeds the model with vertical winglet (0 cant angle) and 30 degree exhibits strong anti stall characteristics. 60 degree winglet cant angle is not a desirable fitment.

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