ISAR Imaging of maneuvering Targets based on a new Algorithm Modified Fast Chirp Fourier Transform for Cubic Chirps

Anitha G¹, Ranga Rao K.S² ¹Department of ECE, GIT, GITAM University anithaguttavelli@gmail.com, ²Dept.of ECE, Anits,Visakhapatnam srrkolluri@gmail.com

Abstract- Inverse Synthetic Aperture Radar (ISAR) imaging of targets with complex motions can be modeled as cubic chirps. Modified Discrete Chirp Fourier Transform (MDCFT) is used to process the cubic signal to obtain ISAR image in two dimensions (2D). In this paper, a new algorithm named Modified Fast Chirp Fourier Transform (MFCFT) is proposed. This algorithm gives accurate results as, and the computation time is very much reduced, compared to MDCFT. The simulation is carried out for ship and Airplane targets with different scattering points. The obtained results show an enhancement both in terms of resolution and computation time in the proposed method hence named Modified Fast chirp Fourier Transform.

Keywords: ISAR, MDCFT, MFCFT, RD, RID, RIC.

I.INTRODUCTION

ISAR imaging is used to produce the high resolution images of moving targets. The focused image of targets with uniform motion is obtained by conventional Range Doppler (RD) method [1]. When targets have high complex motions then they can be characterized by second order phase terms and Range Instantaneous Doppler (RID) is used to obtain the image [2]. Several available ISAR imaging approaches have been previously discussed like FFT, Time frequency transform [3,4], Fractional Fourier transform[5], S-method, Clean technique, Wigner Ville distribution[6]. For targets with very high complex motions such as significant angular motions, like, pitch, roll and yaw, the radar azimuth echoes must be modeled as cubic chirp signals and to obtain the image, Range Instantaneous Chirp (RIC) is used. Therefore, the signal processing of cubic chirps is very important in the ISAR imaging. Presently several algorithms are available for cubic chirps like TC Dechirp clean technique, Product High order Matched Phase Transform (PHMT) [7], Discrete chirp Fourier transform, Modified discrete chirp Fourier transform [8-10]. High quality ISAR images can be effectively obtained via the proposed imaging method both by means of resolution and computation time.

II.MODELING FOR CUBIC CHIRP

When very high maneuvering of target takes place, then the phase of the return signal is represented in terms of higher order phase terms or cubic phase terms. The transmitted LFM signal is represented by [11]

$$S(t_{1}, t_{2}) = rect\left(\frac{t_{1}}{T}\right) \exp\left(j2\pi\left(f\left(t\right) + \frac{1}{2}\gamma(t)^{2}\right)\right)$$

$$where \quad rect\left(\frac{t_{1}}{T}\right) = \begin{cases} 1, \ \left|\left(\frac{t_{1}}{T}\right)\right| \le \frac{1}{2} \\ 0, \ \left|\left(\frac{t_{1}}{T}\right)\right| > \frac{1}{2} \end{cases}$$

$$(1)$$

Where f, γ and T, denote the carrier frequency, chirp rate and pulse width respectively, t is the full time given by t_1+t_2 , t_1 being the fast time and t_2 , the slow time. t_2 is given by n/prf and n=0,1,...N. Here, prf is pulse repetition frequency and N is the number of accumulating pulses. The received echo signal is given by

$$S_{i}(t_{1},t_{2}) = \sigma_{i} \operatorname{rect}\left(\frac{t_{1} - 2R_{i}(t_{2})/c}{T}\right) \exp\left(j2\pi\left(f(t - 2R_{i}(t_{2})/c) + \frac{1}{2}\gamma(t - 2R_{i}(t_{2})/c)^{2}\right)\right)$$
(2)

where $R_i(t_2)$ is the distance between ith scatter and Radar at time t_2 and σ_i represents the reflection coefficient. For this received signal keystone formatting is applied to remove the migration through range cell [12]. Assume that if the number of scatters in a certain range bin is I, the azimuth echoes corresponding to this range bin is expressed as the cubic phase signal [13-18]. The azimuth echo signal is written as

$$S'(t_{2}) = \sum_{i=1}^{I} A_{i} \exp\left[j\left(\theta_{i} + 2\pi\left(f_{i}t_{2} + \frac{1}{2}\gamma_{i}t_{2}^{2} + \frac{1}{6}\beta_{i}t_{2}^{3}\right)\right)\right]$$

$$\theta_{i} = -\left(\frac{4\pi}{\lambda}\right)R_{i}(t_{0})$$

$$f_{i} = -\frac{2}{\lambda}(\omega r^{T})$$

$$\gamma_{i} = -\frac{2}{\lambda}(\alpha r^{T})$$

$$\beta_{i} = -\frac{2}{\lambda}(\zeta r^{T})$$

(3)

where A_i denote the amplitude, θ_i the initial phase, f_i the center frequency, α_i the chirp rate, and β_i is derivative of chirp rate of azimuth echoes associated with the ith scatter respectively. $R_i(t_0)$ is initial range at time t_0 . Therefore, the discrete expression of $S'(t_2)$ is S(n) and is given by

$$S(n) = \sum_{i=1}^{I} A_{i} W_{N}^{f_{i}n + \left(\frac{\gamma_{i}}{N}\right)n^{2} + \left(\frac{\beta_{i}}{N^{2}}\right)n^{3}}$$
(4)

where

$$W_{N} = \exp\left(\frac{-j2\pi}{N}\right), \ A_{i} = a_{i} \exp\left(-j\frac{4\pi}{\lambda}\right)R_{i}(t_{0}), \ f_{i} = \left(\frac{2\omega r^{T}}{\lambda}\right)\left(\frac{N}{prf}\right)$$

$$\gamma_{i} = \left(\frac{\alpha r^{T}}{\lambda}\right)\left(\frac{N^{2}}{prf}\right), \ \beta_{i} = \left(\frac{\zeta r^{T}}{3\lambda}\right)\left(\frac{N^{3}}{prf^{2}}\right),$$
(5)

III.ALGORITHMS FOR RIC

To process the received echo signal for cubic chirps after MTRC, some transforms has to be used in order to obtain the final ISAR image in 2D. Discrete chirp Fourier transform and MDCFT have been used in the recent times to obtain the image. Following sections detail the three methods including the proposed one i.e., DCFT, MDCFT and MFCFT. A comparison of the three methods is also presented.

A. DCFT

DCFT was developed for quadratic terms and extended for cubic chirps which is represented by [11]

$$X(k,l,m) = \frac{1}{\sqrt{N}} \sum_{n=0}^{N-1} x(n) W_N^{kn+\ln^2 + mn^3}$$

$$0 \le k, l, m \le N - 1$$
(6)

where x(n) is chirp signal having signal length N and k, l and m represent the constant frequency, chirp rate and derivative of chirp rate respectively. If the signal parameters are not integers or not very close to integers then, DCFT will suffer from the picket-fence effect. In DCFT since k, l, m values lies in between 0 to N-1, the parameter estimation will not be accurate. Depending on the basic properties of DCFT, if N is a prime number then only the peak is clearly identified and if it is not prime then it leads to picket fence output.

For example consider the two cases.

Case (i). If k=36, l=98, m=25 and N=127(prime number) then the output for DCFT is shown in Fig.1.



Fig.1. Three dimensional plot for DCFT when N=127

Case (ii). If k=36, l=98, m=25 and N=128(not prime number) then the picket fence output is observed for DCFT in Fig.2.



Fig.2 Three dimensional plot for DCFT for N=128

From above Figs.1&2, one can say that DCFT has a limitation in identifying the peak if N is non prime value. To avoid the severe picket-fence effect and increase the accuracy of parameter estimation, MDCFT is proposed.

B. MDCFT

MDCFT for cubic chirp signals is given by [11,19,20]

$$X(k,l,m) = \frac{1}{\sqrt{N}} \sum_{n=0}^{N-1} x(n) W_N^{kn+(l/N)n^2 + (m/N^2)n^3}$$

$$0 \le k, l, m \le N - 1$$
(7)

The parameter estimation in MDCFT is from k $\mathcal{E}(0,1,...N-1)$, l $\mathcal{E}(0,1/N,...(N-1)/N)$, m $\mathcal{E}(0,1/N^2,...(N-1)/N^2)$. Therefore, as the accuracy increases, a shorter near the peak sample interval can be obtained, and MDCFT will not suffer from picket-fence effect. This is verified with the below example.

If k=36, l=98, m=25 and N=128 then the output for MDCFT is shown in Fig.3. From Fig.3, it can be said that the peak is clearly identified.



Fig.3.Three dimensional plot for MDCFT when N=128

The ISAR imaging based on MDCFT for cubic chirps is implemented with the following steps as follows:

i. After applying MDCFT to (7) i.e., s(n) in each range bin, the equation is given by

$$S(k,l,m) = \frac{1}{\sqrt{N}} \sum_{n=0}^{N-1} s(n) W_N^{kn+(l/N)n^2 + (m/N^2)n^3}$$
(8)

where S(k,l,m) is the MDCFT of s(n).

ii. The projection of S(k,l,m) will produce a Doppler image in 3D with center frequency f_i.

iii. Doppler image $I_D(k)$ can be obtained by the energy accumulation along axes of l and m given by

$$I_D(k) = \left| \sum_{l,k} S(k,l,m) \right| \tag{9}$$

In this Doppler image $I_D(k)$ all the main lobes of S(k,l,m) are clearly identified.

- iv. Now the Doppler images of all range bins are added to form the Range Doppler image of the target for cubic chirp signal.
- C. Proposed Algorithm-MFCFT

In MFCFT the representation for cubic chirps is given by

$$X(k,l,m) = \frac{1}{\sqrt{N}} \sum_{n=0}^{N-1} x(n) W_N^{kn+(l/N)n^2+(m/N)n^3}$$

$$0 \le k, l, m \le N-1$$
(10)

where k, l and m represent constant frequency, chirp rate and derivative of chirp rate respectively. Here, the parameters k,l,m are estimated as k $\mathcal{E}(0,1,\dots,N-1)$, l $\mathcal{E}(0,1/N,\dots,(N-1)/N)$, m $\mathcal{E}(0,1/N,\dots,(N-1)/N)$. Therefore it increases the accuracy and near the peak value is identified. This is clearly shown in case (i & ii).

Case i. If k=36, l=98, m=25 and signal length N=127 then the output for MFCFT is shown in Fig.4





Case (ii). If k=36, l=98 and m=25 and signal length N=128 then the peak is clearly identified as shown in Fig.5



Fig.5. Three dimensional plot for MFCFT for N=128

From the figures one can say that the peak is clearly identified in the two cases irrespective of signal length being prime number or not. The ISAR imaging based on MFCFT for cubic chirps is implemented as follows:

i. MFCFT equation given in (10) is applied to s(n) in each range bin, to get S(k,l,m) given by

$$S(k,l,m) = \frac{1}{\sqrt{N}} \sum_{n=0}^{N-1} s(n) W_N^{kn+(l/N)n^2 + (m/N)n^3}$$
(11)

where S(k,l,m) is the MFCFT of s(n).

- ii. The projection of S(k,l,m) will produce a Doppler image in 3D with center frequency f_i .
- iii. Doppler image $I_D(k)$ can be obtained by the energy accumulation along axes of l and m given by

$$I_{D}(k) = \left| \sum_{l,k} S(k,l,m) \right|$$
(12)

In this Doppler image $I_D(k)$ all the main lobes of S(k,l,m) are clearly identified.

- iv. Now the Doppler images of all range bins are added to form the ISAR image of the target for cubic chirp signal.
- v. It may be noted that the proposed algorithm will be found to be more and more effective as higher and higher order terms are considered because exponent of N is defered with.

In this way the 2D ISAR image is obtained for MFCFT where the computation time is very much reduced when compared to MDCFT.

IV.SIMULATION RESULTS

The simulation parameters used in the programming are given in Table. I

Parameter	Representation	Value
Signal length	Ν	150
Bandwidth	BW	384 MHz
Pulse repetition frequency	prf	100Hz
Initial range	R_0	45kms
Frequency	f	5.2GHz
Constant terms	$\omega_1\omega_2 \ \omega_3$	[0.5 0.3 0.6]
First order terms	$\alpha_1 \alpha_2 \alpha_3$	[0.6 0.2 0.5]
Second order terms	$\gamma_1 \gamma_2 \gamma_3$	[0.4 0.5 0.6]
No of scatters		85 and 84

TABLE.I SIMULATION PARAMETERS

Here the simulation has been carried out initially for a ship target with 85 scattering points and for Airplane target with 84 scattering points.

Case i. Simulated ship target is shown in Fig.6. The amplitudes of all the echoes are considered as equal. ISAR image in 2D obtained using MDCFT is shown in Fig.7 and that using MFCFT is shown in Fig.8. In both the cases, the hot spots are clearly identified, but, in case of MFCFT the simulation time is very much reduced when compared to MDCFT.

Case ii. Here an Airplane with 84 scatters is considered as shown in Fig.9. The ISAR image using MDCFT is shown in Fig.10 and that using MFCFT is shown in Fig.11. Here also the hot spots are observed clearly in the two methods but the computation time is reduced in MFCFT.



Fig.6 Simulated ship target with 85 scattering points



Fig.7. ISAR image of ship target using MDCFT



Fig.8. ISAR image of ship target using MFCFT



Fig.9 Simulated Airplane target with 84 scattering points



Fig.10. ISAR image of Airplane target using MDCFT



Fig.11.ISAR image of Airplane target using MFCFT

V. CONCLUSIONS

In this paper, ISAR imaging using MFCFT is discussed for cubic chirp signals. The quality of the image obtained in MFCFT is comparable with that of MDCFT. Additionally the computation time is significantly reduced here. This method will be found to be more effective as higher and higher order terms need to be considered. The advantage in this method is that exponent terms of the signal length remain to be unity.

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AUTHOR PROFILE

Anitha. G graduated in E.C.E from JNTU University in 2006 and did her Master's degree in RF and Microwave from Andhra University in 2008. She is presently working as Assistant Professor in Dept. of E.C.E in GITAM Institute of Technology, GITAM university since 2008 till date. Her areas of interest are Radars, signal processing, etc.

Dr. K. S. RangaRao graduated in Electronics and Communication Engineering from College of Engineering, Kakinada, JNTU Hyderabad in 1977 and Ph.D in Engineering from Electronics and Telecommunication Engineering Department of Jadavpur University, Kolkata in 1994. After having been in IIT, Kharagpur from 1982 to 1996, he joined as a Scientist in Integrated Test Range, Chandipur from 1997 to 2006. He then worked with Naval Science and Technological Laboratory, Visakhapatnam from 2006 to 2015. He is presently working as Professor in the Department of ECE in ANITS Engineering College. His area of work includes RF and Microwave Engineering, Antennas, RADAR & LASER Engineering.